



**NAMIBIA UNIVERSITY  
OF SCIENCE AND TECHNOLOGY**

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<b>QUALIFICATION:</b> BACHELOR OF SCIENCE IN APPLIED MATHEMATICS AND STATISTICS		
<b>QUALIFICATION CODE:</b>	07BAMS	<b>LEVEL:</b> 7
<b>COURSE :</b>	DESIGN AND ANALYSIS OF EXPERIMENT	<b>COURSE CODE:</b> DAE702S
<b>DATE :</b>	JAN 2024	<b>SESSION:</b> 2
<b>DURATION :</b>	3 HOURS	<b>MARKS:</b> 100

<b>SUPPLEMENTARY/ 2ND OPPORTUNITY EXAMINATION QUESTION PAPER</b>	
<b>EXAMINER</b>	Dr. Jacob Ong'ala
<b>MODERATOR</b>	Dr Petrus Iiyambo

#### **INSTRUCTION**

1. Answer all questions on the separate answer sheet.
2. Please write neatly and legibly.
3. Do not use the left side margin of the exam paper. This must be allowed for the examiner.
4. No books, notes and other additional aids are allowed.
5. Mark all answers clearly with their respective question numbers.

#### **PERMISSIBLE MATERIALS**

1. Non-Programmable Calculator

#### **ATTACHEMENTS**

1. F distribution table
2. OC Curves for the Fixed model Analysis of Variance
3. t distribution table

**THIS QUESTION PAPER CONSISTS OF 4 PAGES**  
(including the front page)

**QUESTION ONE - 28 MARKS**

- (a) Consider an experiment of two factor (A and B). Each factors has two levels (low and High). the response for the experiment is shown in the table below.

		Factor B	
		Low	High
Factor A	Low	20	40
	High	50	12

- (i) Compute main effect of factor A [1 mks]  
 (ii) Compute main effect of factor B [1 mks]  
 (iii) Compute the interaction effect [2 mks]  
 (iv) Draw an interaction plot for the experiment [2 mks]
- (b) Several ovens in a metal working shop are used to heat metal specimens. All the ovens are supposed to operate at the same temperature, although it is suspected that this may not be true. Three ovens are selected at random, and their temperatures on successive heats are noted. The data collected are as follows:(Use  $\alpha = 0.05$ )

Oven	Temperature					
1	491.50	498.30	498.10	493.50	493.60	
2	488.50	484.65	479.90	477.35		
3	490.10	484.80	488.25	473.00	471.85	478.65

- (i) Construct ANOVA table [12 mks]  
 (ii) Formulate the hypothesis when random effect model is assumed [2 mks]  
 (iii) What do you conclude from the ANOVA table above? [3 mks]  
 (iv) Estimate variance component [5 mks]

**QUESTION TWO - 22 MARKS**

Suppose that four normal populations have means of  $\mu_1 = 50$ ,  $\mu_2 = 60$ ,  $\mu_3 = 50$ , and  $\mu_4 = 60$ .

- (a) How many observations should be taken from each population so that the probability of rejecting the null hypothesis of equal population means is at least 0.90? Assume that  $\alpha = 0.05$  and that a reasonable estimate of the error variance is  $\sigma^2 = 25$ . [10 mks]  
 (b) How would your answer change if a reasonable estimate of the experimental error variance were  $\sigma^2 = 36$  [5 mks]  
 (c) How would your answer change if a reasonable estimate of the experimental error variance were  $\sigma^2 = 49$  [5 mks]

- (d) Can you draw any conclusions about the sensitivity of your answer in this particular situation about how your estimate of  $\sigma$  affects the decision about sample size? [2 mks]

**QUESTION THREE - 28 MARKS**

- (a) The ANOVA from a randomized complete block experiment output is shown below.

Source	DF	SS	MS	F	P
Treatment	4	1010.56	?	29.84	?
Block	?	?	64.765	?	?
Error	20	169.33	?		
Total	29	1503.71			

- (i) Fill in the blanks [4 mks]  
(ii) How many blocks were used in this experiment? [1 mks]  
(iii) What conclusions can you draw? [2 mks]
- (b) A chemist wishes to test the effect of four chemical agents on the strength of a particular type of cloth. Because there might be variability from one bolt to another, the chemist decides to use a randomized block design, with the bolts of cloth considered as blocks. She selects five bolts and applies all four chemicals in random order to each bolt. The resulting tensile strengths are as follow

Chemical	Bolt				
	1	2	3	4	5
1	73	68	74	71	67
2	73	67	75	72	70
3	75	68	78	73	68
4	73	71	75	75	69

- (i) Analyze the data from this experiment. [12 mks]  
(ii) Use the Fisher LSD method to make comparisons among the four Chemicals [9 mks]

**QUESTION FOUR - 22 MARKS**

The survival times of group of four beetles randomly allocated to twelve treatments groups obtained by crossing the levels of four insecticides (A,B,C,D) at each of three concentrations of the insecticides (1=low, 2=Medium, 3=High) is shown in the table below. This is a balanced 4-by-3 factorial design (two-factor design) that is replicated 4 times

Dose	Insecticide	Survival Times			
1	A	.31	.45	.46	.43
	B	.88	1.10	.88	.77
	C	.44	.45	.63	.76
	D	.44	.71	.60	.62
2	A	.93	.29	.40	.23
	B	.92	.61	.49	1.24
	C	.44	.35	.31	.40
	D	.51	1.02	.71	.38
3	A	.22	.21	.18	.23
	B	.30	.37	.30	.29
	C	.23	.25	.24	.22
	D	.30	.36	.31	.33

- (a) Formulate the hypotheses for this experiment [2 mks]
- (b) Test the hypothesis above using Analysis of Variance [16 mks]
- (c) What do you conclude from the ANOVA results above [4 mks]

- END OF QUESTIONS -



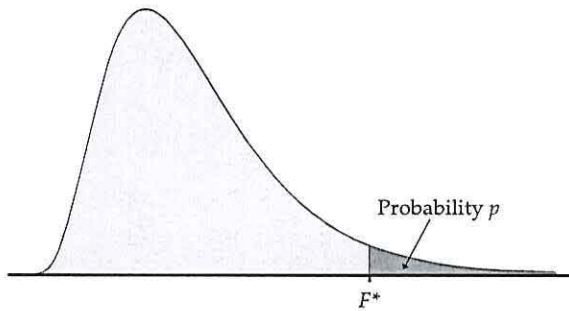


Table entry for  $p$  is the critical value  $F^*$  with probability  $p$  lying to its right.

**TABLE E**  
F critical values

		Degrees of freedom in the numerator								
		1	2	3	4	5	6	7	8	9
Degrees of freedom in the denominator	$p$									
	1	.100	39.86	49.50	53.59	55.83	57.24	58.20	58.91	59.44
.050		161.45	199.50	215.71	224.58	230.16	233.99	236.77	238.88	240.54
.025		647.79	799.50	864.16	899.58	921.85	937.11	948.22	956.66	963.28
.010		4052.2	4999.5	5403.4	5624.6	5763.6	5859.0	5928.4	5981.1	6022.5
	.001	405284	500000	540379	562500	576405	585937	592873	598144	602284
2	.100	8.53	9.00	9.16	9.24	9.29	9.33	9.35	9.37	9.38
	.050	18.51	19.00	19.16	19.25	19.30	19.33	19.35	19.37	19.38
	.025	38.51	39.00	39.17	39.25	39.30	39.33	39.36	39.37	39.39
	.010	98.50	99.00	99.17	99.25	99.30	99.33	99.36	99.37	99.39
	.001	998.50	999.00	999.17	999.25	999.30	999.33	999.36	999.37	999.39
3	.100	5.54	5.46	5.39	5.34	5.31	5.28	5.27	5.25	5.24
	.050	10.13	9.55	9.28	9.12	9.01	8.94	8.89	8.85	8.81
	.025	17.44	16.04	15.44	15.10	14.88	14.73	14.62	14.54	14.47
	.010	34.12	30.82	29.46	28.71	28.24	27.91	27.67	27.49	27.35
	.001	167.03	148.50	141.11	137.10	134.58	132.85	131.58	130.62	129.86
4	.100	4.54	4.32	4.19	4.11	4.05	4.01	3.98	3.95	3.94
	.050	7.71	6.94	6.59	6.39	6.26	6.16	6.09	6.04	6.00
	.025	12.22	10.65	9.98	9.60	9.36	9.20	9.07	8.98	8.90
	.010	21.20	18.00	16.69	15.98	15.52	15.21	14.98	14.80	14.66
	.001	74.14	61.25	56.18	53.44	51.71	50.53	49.66	49.00	48.47
5	.100	4.06	3.78	3.62	3.52	3.45	3.40	3.37	3.34	3.32
	.050	6.61	5.79	5.41	5.19	5.05	4.95	4.88	4.82	4.77
	.025	10.01	8.43	7.76	7.39	7.15	6.98	6.85	6.76	6.68
	.010	16.26	13.27	12.06	11.39	10.97	10.67	10.46	10.29	10.16
	.001	47.18	37.12	33.20	31.09	29.75	28.83	28.16	27.65	27.24
6	.100	3.78	3.46	3.29	3.18	3.11	3.05	3.01	2.98	2.96
	.050	5.99	5.14	4.76	4.53	4.39	4.28	4.21	4.15	4.10
	.025	8.81	7.26	6.60	6.23	5.99	5.82	5.70	5.60	5.52
	.010	13.75	10.92	9.78	9.15	8.75	8.47	8.26	8.10	7.98
	.001	35.51	27.00	23.70	21.92	20.80	20.03	19.46	19.03	18.69
7	.100	3.59	3.26	3.07	2.96	2.88	2.83	2.78	2.75	2.72
	.050	5.59	4.74	4.35	4.12	3.97	3.87	3.79	3.73	3.68
	.025	8.07	6.54	5.89	5.52	5.29	5.12	4.99	4.90	4.82
	.010	12.25	9.55	8.45	7.85	7.46	7.19	6.99	6.84	6.72
	.001	29.25	21.69	18.77	17.20	16.21	15.52	15.02	14.63	14.33

Table entry for  $p$  is the critical value  $F^*$  with probability  $p$  lying to its right.

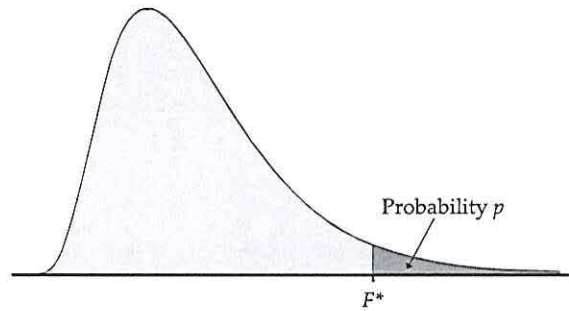


TABLE E										
F critical values (continued)										
Degrees of freedom in the numerator										
10	12	15	20	25	30	40	50	60	120	1000
60.19	60.71	61.22	61.74	62.05	62.26	62.53	62.69	62.79	63.06	63.30
241.88	243.91	245.95	248.01	249.26	250.10	251.14	251.77	252.20	253.25	254.19
968.63	976.71	984.87	993.10	998.08	1001.4	1005.6	1008.1	1009.8	1014.0	1017.7
6055.8	6106.3	6157.3	6208.7	6239.8	6260.6	6286.8	6302.5	6313.0	6339.4	6362.7
605621	610668	615764	620908	624017	626099	628712	630285	631337	633972	636301
9.39	9.41	9.42	9.44	9.45	9.46	9.47	9.47	9.47	9.48	9.49
19.40	19.41	19.43	19.45	19.46	19.46	19.47	19.48	19.48	19.49	19.49
39.40	39.41	39.43	39.45	39.46	39.46	39.47	39.48	39.48	39.49	39.50
99.40	99.42	99.43	99.45	99.46	99.47	99.47	99.48	99.48	99.49	99.50
999.40	999.42	999.43	999.45	999.46	999.47	999.47	999.48	999.48	999.49	999.50
5.23	5.22	5.20	5.18	5.17	5.17	5.16	5.15	5.15	5.14	5.13
8.79	8.74	8.70	8.66	8.63	8.62	8.59	8.58	8.57	8.55	8.53
14.42	14.34	14.25	14.17	14.12	14.08	14.04	14.01	13.99	13.95	13.91
27.23	27.05	26.87	26.69	26.58	26.50	26.41	26.35	26.32	26.22	26.14
129.25	128.32	127.37	126.42	125.84	125.45	124.96	124.66	124.47	123.97	123.53
3.92	3.90	3.87	3.84	3.83	3.82	3.80	3.80	3.79	3.78	3.76
5.96	5.91	5.86	5.80	5.77	5.75	5.72	5.70	5.69	5.66	5.63
8.84	8.75	8.66	8.56	8.50	8.46	8.41	8.38	8.36	8.31	8.26
14.55	14.37	14.20	14.02	13.91	13.84	13.75	13.69	13.65	13.56	13.47
48.05	47.41	46.76	46.10	45.70	45.43	45.09	44.88	44.75	44.40	44.09
3.30	3.27	3.24	3.21	3.19	3.17	3.16	3.15	3.14	3.12	3.11
4.74	4.68	4.62	4.56	4.52	4.50	4.46	4.44	4.43	4.40	4.37
6.62	6.52	6.43	6.33	6.27	6.23	6.18	6.14	6.12	6.07	6.02
10.05	9.89	9.72	9.55	9.45	9.38	9.29	9.24	9.20	9.11	9.03
26.92	26.42	25.91	25.39	25.08	24.87	24.60	24.44	24.33	24.06	23.82
2.94	2.90	2.87	2.84	2.81	2.80	2.78	2.77	2.76	2.74	2.72
4.06	4.00	3.94	3.87	3.83	3.81	3.77	3.75	3.74	3.70	3.67
5.46	5.37	5.27	5.17	5.11	5.07	5.01	4.98	4.96	4.90	4.86
7.87	7.72	7.56	7.40	7.30	7.23	7.14	7.09	7.06	6.97	6.89
18.41	17.99	17.56	17.12	16.85	16.67	16.44	16.31	16.21	15.98	15.77
2.70	2.67	2.63	2.59	2.57	2.56	2.54	2.52	2.51	2.49	2.47
3.64	3.57	3.51	3.44	3.40	3.38	3.34	3.32	3.30	3.27	3.23
4.76	4.67	4.57	4.47	4.40	4.36	4.31	4.28	4.25	4.20	4.15
6.62	6.47	6.31	6.16	6.06	5.99	5.91	5.86	5.82	5.74	5.66
14.08	13.71	13.32	12.93	12.69	12.53	12.33	12.20	12.12	11.91	11.72

(Continued)

**TABLE E**  
*F* critical values (continued)

		Degrees of freedom in the numerator										
		1	2	3	4	5	6	7	8	9		
<i>p</i>												
Degrees of freedom in the denominator	8	.100	3.46	3.11	2.92	2.81	2.73	2.67	2.62	2.59	2.56	
		.050	5.32	4.46	4.07	3.84	3.69	3.58	3.50	3.44	3.39	
		.025	7.57	6.06	5.42	5.05	4.82	4.65	4.53	4.43	4.36	
		.010	11.26	8.65	7.59	7.01	6.63	6.37	6.18	6.03	5.91	
		.001	25.41	18.49	15.83	14.39	13.48	12.86	12.40	12.05	11.77	
		9	.100	3.36	3.01	2.81	2.69	2.61	2.55	2.51	2.47	2.44
		.050	5.12	4.26	3.86	3.63	3.48	3.37	3.29	3.23	3.18	
		.025	7.21	5.71	5.08	4.72	4.48	4.32	4.20	4.10	4.03	
		.010	10.56	8.02	6.99	6.42	6.06	5.80	5.61	5.47	5.35	
		.001	22.86	16.39	13.90	12.56	11.71	11.13	10.70	10.37	10.11	
		10	.100	3.29	2.92	2.73	2.61	2.52	2.46	2.41	2.38	2.35
		.050	4.96	4.10	3.71	3.48	3.33	3.22	3.14	3.07	3.02	
		.025	6.94	5.46	4.83	4.47	4.24	4.07	3.95	3.85	3.78	
		.010	10.04	7.56	6.55	5.99	5.64	5.39	5.20	5.06	4.94	
		.001	21.04	14.91	12.55	11.28	10.48	9.93	9.52	9.20	8.96	
		11	.100	3.23	2.86	2.66	2.54	2.45	2.39	2.34	2.30	2.27
		.050	4.84	3.98	3.59	3.36	3.20	3.09	3.01	2.95	2.90	
	.025	6.72	5.26	4.63	4.28	4.04	3.88	3.76	3.66	3.59		
	.010	9.65	7.21	6.22	5.67	5.32	5.07	4.89	4.74	4.63		
	.001	19.69	13.81	11.56	10.35	9.58	9.05	8.66	8.35	8.12		
	12	.100	3.18	2.81	2.61	2.48	2.39	2.33	2.28	2.24	2.21	
	.050	4.75	3.89	3.49	3.26	3.11	3.00	2.91	2.85	2.80		
	.025	6.55	5.10	4.47	4.12	3.89	3.73	3.61	3.51	3.44		
	.010	9.33	6.93	5.95	5.41	5.06	4.82	4.64	4.50	4.39		
	.001	18.64	12.97	10.80	9.63	8.89	8.38	8.00	7.71	7.48		
	13	.100	3.14	2.76	2.56	2.43	2.35	2.28	2.23	2.20	2.16	
	.050	4.67	3.81	3.41	3.18	3.03	2.92	2.83	2.77	2.71		
	.025	6.41	4.97	4.35	4.00	3.77	3.60	3.48	3.39	3.31		
	.010	9.07	6.70	5.74	5.21	4.86	4.62	4.44	4.30	4.19		
	.001	17.82	12.31	10.21	9.07	8.35	7.86	7.49	7.21	6.98		
	14	.100	3.10	2.73	2.52	2.39	2.31	2.24	2.19	2.15	2.12	
	.050	4.60	3.74	3.34	3.11	2.96	2.85	2.76	2.70	2.65		
	.025	6.30	4.86	4.24	3.89	3.66	3.50	3.38	3.29	3.21		
	.010	8.86	6.51	5.56	5.04	4.69	4.46	4.28	4.14	4.03		
	.001	17.14	11.78	9.73	8.62	7.92	7.44	7.08	6.80	6.58		
	15	.100	3.07	2.70	2.49	2.36	2.27	2.21	2.16	2.12	2.09	
	.050	4.54	3.68	3.29	3.06	2.90	2.79	2.71	2.64	2.59		
	.025	6.20	4.77	4.15	3.80	3.58	3.41	3.29	3.20	3.12		
	.010	8.68	6.36	5.42	4.89	4.56	4.32	4.14	4.00	3.89		
	.001	16.59	11.34	9.34	8.25	7.57	7.09	6.74	6.47	6.26		
	16	.100	3.05	2.67	2.46	2.33	2.24	2.18	2.13	2.09	2.06	
	.050	4.49	3.63	3.24	3.01	2.85	2.74	2.66	2.59	2.54		
	.025	6.12	4.69	4.08	3.73	3.50	3.34	3.22	3.12	3.05		
	.010	8.53	6.23	5.29	4.77	4.44	4.20	4.03	3.89	3.78		
	.001	16.12	10.97	9.01	7.94	7.27	6.80	6.46	6.19	5.98		
	17	.100	3.03	2.64	2.44	2.31	2.22	2.15	2.10	2.06	2.03	
	.050	4.45	3.59	3.20	2.96	2.81	2.70	2.61	2.55	2.49		
	.025	6.04	4.62	4.01	3.66	3.44	3.28	3.16	3.06	2.98		
	.010	8.40	6.11	5.19	4.67	4.34	4.10	3.93	3.79	3.68		
	.001	15.72	10.66	8.73	7.68	7.02	6.56	6.22	5.96	5.75		



**TABLE E**

*F* critical values (continued)

Degrees of freedom in the numerator										
10	12	15	20	25	30	40	50	60	120	1000
2.54	2.50	2.46	2.42	2.40	2.38	2.36	2.35	2.34	2.32	2.30
3.35	3.28	3.22	3.15	3.11	3.08	3.04	3.02	3.01	2.97	2.93
4.30	4.20	4.10	4.00	3.94	3.89	3.84	3.81	3.78	3.73	3.68
5.81	5.67	5.52	5.36	5.26	5.20	5.12	5.07	5.03	4.95	4.87
11.54	11.19	10.84	10.48	10.26	10.11	9.92	9.80	9.73	9.53	9.36
2.42	2.38	2.34	2.30	2.27	2.25	2.23	2.22	2.21	2.18	2.16
3.14	3.07	3.01	2.94	2.89	2.86	2.83	2.80	2.79	2.75	2.71
3.96	3.87	3.77	3.67	3.60	3.56	3.51	3.47	3.45	3.39	3.34
5.26	5.11	4.96	4.81	4.71	4.65	4.57	4.52	4.48	4.40	4.32
9.89	9.57	9.24	8.90	8.69	8.55	8.37	8.26	8.19	8.00	7.84
2.32	2.28	2.24	2.20	2.17	2.16	2.13	2.12	2.11	2.08	2.06
2.98	2.91	2.85	2.77	2.73	2.70	2.66	2.64	2.62	2.58	2.54
3.72	3.62	3.52	3.42	3.35	3.31	3.26	3.22	3.20	3.14	3.09
4.85	4.71	4.56	4.41	4.31	4.25	4.17	4.12	4.08	4.00	3.92
8.75	8.45	8.13	7.80	7.60	7.47	7.30	7.19	7.12	6.94	6.78
2.25	2.21	2.17	2.12	2.10	2.08	2.05	2.04	2.03	2.00	1.98
2.85	2.79	2.72	2.65	2.60	2.57	2.53	2.51	2.49	2.45	2.41
3.53	3.43	3.33	3.23	3.16	3.12	3.06	3.03	3.00	2.94	2.89
4.54	4.40	4.25	4.10	4.01	3.94	3.86	3.81	3.78	3.69	3.61
7.92	7.63	7.32	7.01	6.81	6.68	6.52	6.42	6.35	6.18	6.02
2.19	2.15	2.10	2.06	2.03	2.01	1.99	1.97	1.96	1.93	1.91
2.75	2.69	2.62	2.54	2.50	2.47	2.43	2.40	2.38	2.34	2.30
3.37	3.28	3.18	3.07	3.01	2.96	2.91	2.87	2.85	2.79	2.73
4.30	4.16	4.01	3.86	3.76	3.70	3.62	3.57	3.54	3.45	3.37
7.29	7.00	6.71	6.40	6.22	6.09	5.93	5.83	5.76	5.59	5.44
2.14	2.10	2.05	2.01	1.98	1.96	1.93	1.92	1.90	1.88	1.85
2.67	2.60	2.53	2.46	2.41	2.38	2.34	2.31	2.30	2.25	2.21
3.25	3.15	3.05	2.95	2.88	2.84	2.78	2.74	2.72	2.66	2.60
4.10	3.96	3.82	3.66	3.57	3.51	3.43	3.38	3.34	3.25	3.18
6.80	6.52	6.23	5.93	5.75	5.63	5.47	5.37	5.30	5.14	4.99
2.10	2.05	2.01	1.96	1.93	1.91	1.89	1.87	1.86	1.83	1.80
2.60	2.53	2.46	2.39	2.34	2.31	2.27	2.24	2.22	2.18	2.14
3.15	3.05	2.95	2.84	2.78	2.73	2.67	2.64	2.61	2.55	2.50
3.94	3.80	3.66	3.51	3.41	3.35	3.27	3.22	3.18	3.09	3.02
6.40	6.13	5.85	5.56	5.38	5.25	5.10	5.00	4.94	4.77	4.62
2.06	2.02	1.97	1.92	1.89	1.87	1.85	1.83	1.82	1.79	1.76
2.54	2.48	2.40	2.33	2.28	2.25	2.20	2.18	2.16	2.11	2.07
3.06	2.96	2.86	2.76	2.69	2.64	2.59	2.55	2.52	2.46	2.40
3.80	3.67	3.52	3.37	3.28	3.21	3.13	3.08	3.05	2.96	2.88
6.08	5.81	5.54	5.25	5.07	4.95	4.80	4.70	4.64	4.47	4.33
2.03	1.99	1.94	1.89	1.86	1.84	1.81	1.79	1.78	1.75	1.72
2.49	2.42	2.35	2.28	2.23	2.19	2.15	2.12	2.11	2.06	2.02
2.99	2.89	2.79	2.68	2.61	2.57	2.51	2.47	2.45	2.38	2.32
3.69	3.55	3.41	3.26	3.16	3.10	3.02	2.97	2.93	2.84	2.76
5.81	5.55	5.27	4.99	4.82	4.70	4.54	4.45	4.39	4.23	4.08
2.00	1.96	1.91	1.86	1.83	1.81	1.78	1.76	1.75	1.72	1.69
2.45	2.38	2.31	2.23	2.18	2.15	2.10	2.08	2.06	2.01	1.97
2.92	2.82	2.72	2.62	2.55	2.50	2.44	2.41	2.38	2.32	2.26
3.59	3.46	3.31	3.16	3.07	3.00	2.92	2.87	2.83	2.75	2.66
5.58	5.32	5.05	4.78	4.60	4.48	4.33	4.24	4.18	4.02	3.87

(Continued)



**TABLE E**

*F* critical values (continued)

		Degrees of freedom in the numerator										
<i>p</i>		1	2	3	4	5	6	7	8	9		
Degrees of freedom in the denominator	18	.100	3.01	2.62	2.42	2.29	2.20	2.13	2.08	2.04	2.00	
		.050	4.41	3.55	3.16	2.93	2.77	2.66	2.58	2.51	2.46	
		.025	5.98	4.56	3.95	3.61	3.38	3.22	3.10	3.01	2.93	
		.010	8.29	6.01	5.09	4.58	4.25	4.01	3.84	3.71	3.60	
		.001	15.38	10.39	8.49	7.46	6.81	6.35	6.02	5.76	5.56	
		19	.100	2.99	2.61	2.40	2.27	2.18	2.11	2.06	2.02	1.98
			.050	4.38	3.52	3.13	2.90	2.74	2.63	2.54	2.48	2.42
			.025	5.92	4.51	3.90	3.56	3.33	3.17	3.05	2.96	2.88
			.010	8.18	5.93	5.01	4.50	4.17	3.94	3.77	3.63	3.52
			.001	15.08	10.16	8.28	7.27	6.62	6.18	5.85	5.59	5.39
		20	.100	2.97	2.59	2.38	2.25	2.16	2.09	2.04	2.00	1.96
			.050	4.35	3.49	3.10	2.87	2.71	2.60	2.51	2.45	2.39
			.025	5.87	4.46	3.86	3.51	3.29	3.13	3.01	2.91	2.84
			.010	8.10	5.85	4.94	4.43	4.10	3.87	3.70	3.56	3.46
			.001	14.82	9.95	8.10	7.10	6.46	6.02	5.69	5.44	5.24
		21	.100	2.96	2.57	2.36	2.23	2.14	2.08	2.02	1.98	1.95
			.050	4.32	3.47	3.07	2.84	2.68	2.57	2.49	2.42	2.37
			.025	5.83	4.42	3.82	3.48	3.25	3.09	2.97	2.87	2.80
			.010	8.02	5.78	4.87	4.37	4.04	3.81	3.64	3.51	3.40
			.001	14.59	9.77	7.94	6.95	6.32	5.88	5.56	5.31	5.11
	22	.100	2.95	2.56	2.35	2.22	2.13	2.06	2.01	1.97	1.93	
		.050	4.30	3.44	3.05	2.82	2.66	2.55	2.46	2.40	2.34	
		.025	5.79	4.38	3.78	3.44	3.22	3.05	2.93	2.84	2.76	
		.010	7.95	5.72	4.82	4.31	3.99	3.76	3.59	3.45	3.35	
		.001	14.38	9.61	7.80	6.81	6.19	5.76	5.44	5.19	4.99	
	23	.100	2.94	2.55	2.34	2.21	2.11	2.05	1.99	1.95	1.92	
		.050	4.28	3.42	3.03	2.80	2.64	2.53	2.44	2.37	2.32	
		.025	5.75	4.35	3.75	3.41	3.18	3.02	2.90	2.81	2.73	
		.010	7.88	5.66	4.76	4.26	3.94	3.71	3.54	3.41	3.30	
		.001	14.20	9.47	7.67	6.70	6.08	5.65	5.33	5.09	4.89	
	24	.100	2.93	2.54	2.33	2.19	2.10	2.04	1.98	1.94	1.91	
		.050	4.26	3.40	3.01	2.78	2.62	2.51	2.42	2.36	2.30	
		.025	5.72	4.32	3.72	3.38	3.15	2.99	2.87	2.78	2.70	
		.010	7.82	5.61	4.72	4.22	3.90	3.67	3.50	3.36	3.26	
		.001	14.03	9.34	7.55	6.59	5.98	5.55	5.23	4.99	4.80	
	25	.100	2.92	2.53	2.32	2.18	2.09	2.02	1.97	1.93	1.89	
		.050	4.24	3.39	2.99	2.76	2.60	2.49	2.40	2.34	2.28	
		.025	5.69	4.29	3.69	3.35	3.13	2.97	2.85	2.75	2.68	
		.010	7.77	5.57	4.68	4.18	3.85	3.63	3.46	3.32	3.22	
		.001	13.88	9.22	7.45	6.49	5.89	5.46	5.15	4.91	4.71	
	26	.100	2.91	2.52	2.31	2.17	2.08	2.01	1.96	1.92	1.88	
		.050	4.23	3.37	2.98	2.74	2.59	2.47	2.39	2.32	2.27	
		.025	5.66	4.27	3.67	3.33	3.10	2.94	2.82	2.73	2.65	
		.010	7.72	5.53	4.64	4.14	3.82	3.59	3.42	3.29	3.18	
		.001	13.74	9.12	7.36	6.41	5.80	5.38	5.07	4.83	4.64	
	27	.100	2.90	2.51	2.30	2.17	2.07	2.00	1.95	1.91	1.87	
		.050	4.21	3.35	2.96	2.73	2.57	2.46	2.37	2.31	2.25	
		.025	5.63	4.24	3.65	3.31	3.08	2.92	2.80	2.71	2.63	
		.010	7.68	5.49	4.60	4.11	3.78	3.56	3.39	3.26	3.15	
		.001	13.61	9.02	7.27	6.33	5.73	5.31	5.00	4.76	4.57	

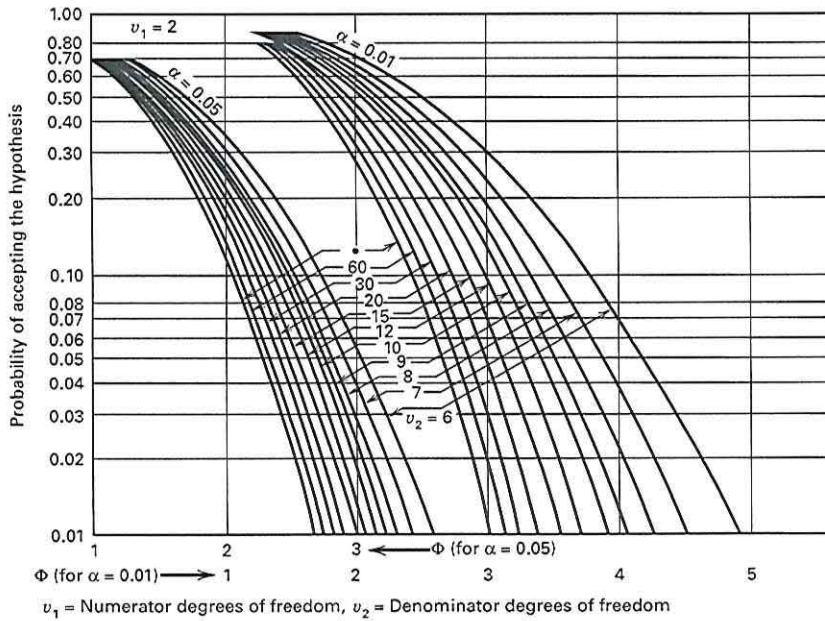
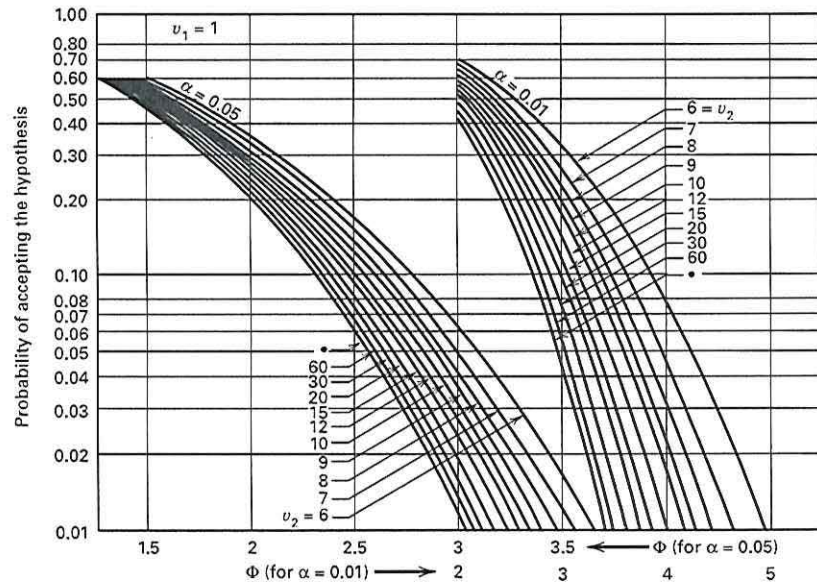
**TABLE E**

F critical values (continued)

Degrees of freedom in the numerator										
10	12	15	20	25	30	40	50	60	120	1000
1.98	1.93	1.89	1.84	1.80	1.78	1.75	1.74	1.72	1.69	1.66
2.41	2.34	2.27	2.19	2.14	2.11	2.06	2.04	2.02	1.97	1.92
2.87	2.77	2.67	2.56	2.49	2.44	2.38	2.35	2.32	2.26	2.20
3.51	3.37	3.23	3.08	2.98	2.92	2.84	2.78	2.75	2.66	2.58
5.39	5.13	4.87	4.59	4.42	4.30	4.15	4.06	4.00	3.84	3.69
1.96	1.91	1.86	1.81	1.78	1.76	1.73	1.71	1.70	1.67	1.64
2.38	2.31	2.23	2.16	2.11	2.07	2.03	2.00	1.98	1.93	1.88
2.82	2.72	2.62	2.51	2.44	2.39	2.33	2.30	2.27	2.20	2.14
3.43	3.30	3.15	3.00	2.91	2.84	2.76	2.71	2.67	2.58	2.50
5.22	4.97	4.70	4.43	4.26	4.14	3.99	3.90	3.84	3.68	3.53
1.94	1.89	1.84	1.79	1.76	1.74	1.71	1.69	1.68	1.64	1.61
2.35	2.28	2.20	2.12	2.07	2.04	1.99	1.97	1.95	1.90	1.85
2.77	2.68	2.57	2.46	2.40	2.35	2.29	2.25	2.22	2.16	2.09
3.37	3.23	3.09	2.94	2.84	2.78	2.69	2.64	2.61	2.52	2.43
5.08	4.82	4.56	4.29	4.12	4.00	3.86	3.77	3.70	3.54	3.40
1.92	1.87	1.83	1.78	1.74	1.72	1.69	1.67	1.66	1.62	1.59
2.32	2.25	2.18	2.10	2.05	2.01	1.96	1.94	1.92	1.87	1.82
2.73	2.64	2.53	2.42	2.36	2.31	2.25	2.21	2.18	2.11	2.05
3.31	3.17	3.03	2.88	2.79	2.72	2.64	2.58	2.55	2.46	2.37
4.95	4.70	4.44	4.17	4.00	3.88	3.74	3.64	3.58	3.42	3.28
1.90	1.86	1.81	1.76	1.73	1.70	1.67	1.65	1.64	1.60	1.57
2.30	2.23	2.15	2.07	2.02	1.98	1.94	1.91	1.89	1.84	1.79
2.70	2.60	2.50	2.39	2.32	2.27	2.21	2.17	2.14	2.08	2.01
3.26	3.12	2.98	2.83	2.73	2.67	2.58	2.53	2.50	2.40	2.32
4.83	4.58	4.33	4.06	3.89	3.78	3.63	3.54	3.48	3.32	3.17
1.89	1.84	1.80	1.74	1.71	1.69	1.66	1.64	1.62	1.59	1.55
2.27	2.20	2.13	2.05	2.00	1.96	1.91	1.88	1.86	1.81	1.76
2.67	2.57	2.47	2.36	2.29	2.24	2.18	2.14	2.11	2.04	1.98
3.21	3.07	2.93	2.78	2.69	2.62	2.54	2.48	2.45	2.35	2.27
4.73	4.48	4.23	3.96	3.79	3.68	3.53	3.44	3.38	3.22	3.08
1.88	1.83	1.78	1.73	1.70	1.67	1.64	1.62	1.61	1.57	1.54
2.25	2.18	2.11	2.03	1.97	1.94	1.89	1.86	1.84	1.79	1.74
2.64	2.54	2.44	2.33	2.26	2.21	2.15	2.11	2.08	2.01	1.94
3.17	3.03	2.89	2.74	2.64	2.58	2.49	2.44	2.40	2.31	2.22
4.64	4.39	4.14	3.87	3.71	3.59	3.45	3.36	3.29	3.14	2.99
1.87	1.82	1.77	1.72	1.68	1.66	1.63	1.61	1.59	1.56	1.52
2.24	2.16	2.09	2.01	1.96	1.92	1.87	1.84	1.82	1.77	1.72
2.61	2.51	2.41	2.30	2.23	2.18	2.12	2.08	2.05	1.98	1.91
3.13	2.99	2.85	2.70	2.60	2.54	2.45	2.40	2.36	2.27	2.18
4.56	4.31	4.06	3.79	3.63	3.52	3.37	3.28	3.22	3.06	2.91
1.86	1.81	1.76	1.71	1.67	1.65	1.61	1.59	1.58	1.54	1.51
2.22	2.15	2.07	1.99	1.94	1.90	1.85	1.82	1.80	1.75	1.70
2.59	2.49	2.39	2.28	2.21	2.16	2.09	2.05	2.03	1.95	1.89
3.09	2.96	2.81	2.66	2.57	2.50	2.42	2.36	2.33	2.23	2.14
4.48	4.24	3.99	3.72	3.56	3.44	3.30	3.21	3.15	2.99	2.84
1.85	1.80	1.75	1.70	1.66	1.64	1.60	1.58	1.57	1.53	1.50
2.20	2.13	2.06	1.97	1.92	1.88	1.84	1.81	1.79	1.73	1.68
2.57	2.47	2.36	2.25	2.18	2.13	2.07	2.03	2.00	1.93	1.86
3.06	2.93	2.78	2.63	2.54	2.47	2.38	2.33	2.29	2.20	2.11
4.41	4.17	3.92	3.66	3.49	3.38	3.23	3.14	3.08	2.92	2.78

(Continued)

V Operating Characteristic Curves for the Fixed Effects Model Analysis of Variance<sup>a</sup>

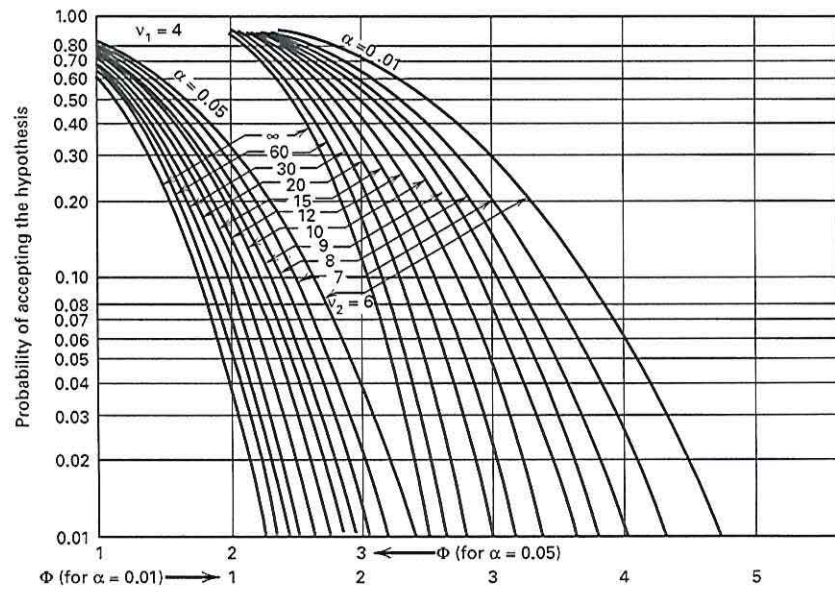
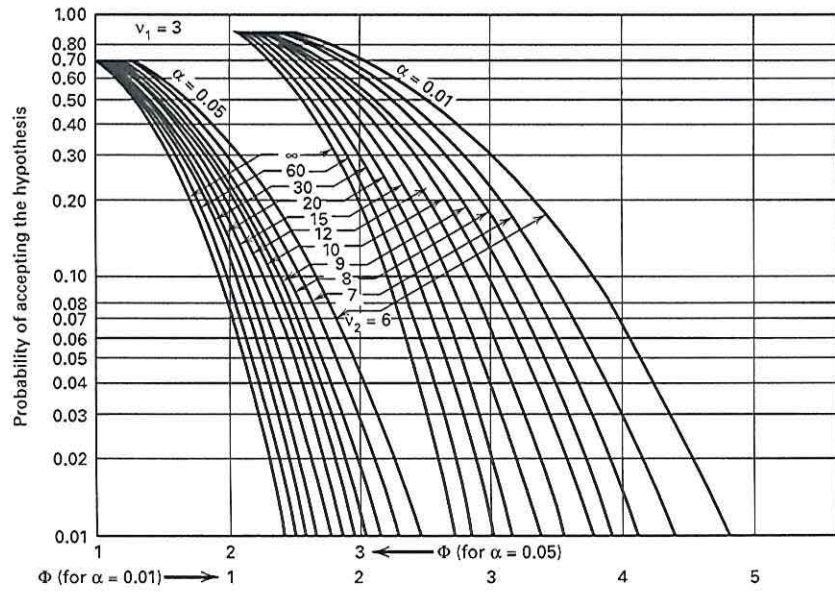


$v_1$  = Numerator degrees of freedom,  $v_2$  = Denominator degrees of freedom

<sup>a</sup>Adapted with permission from *Biometrika Tables for Statisticians*, Vol. 2, by E. S. Pearson and H. O. Hartley, Cambridge University Press, Cambridge, 1972.

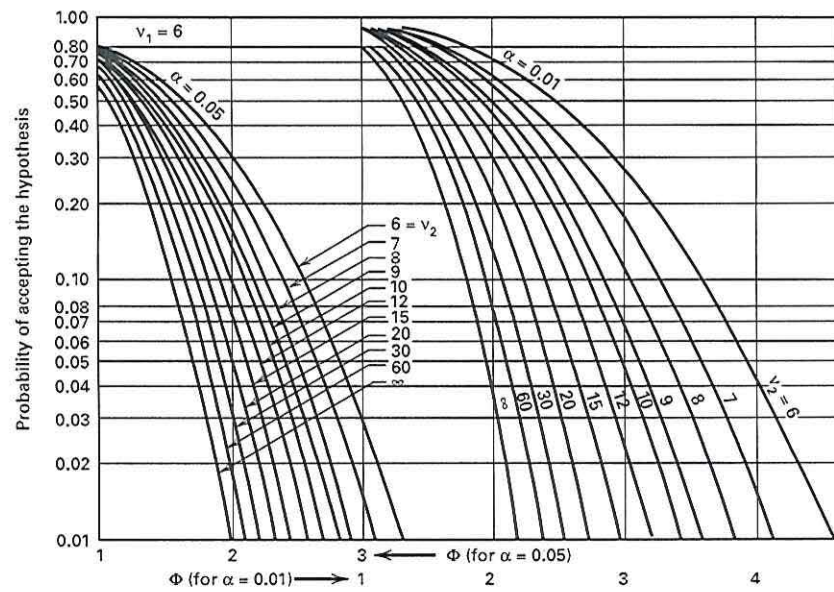
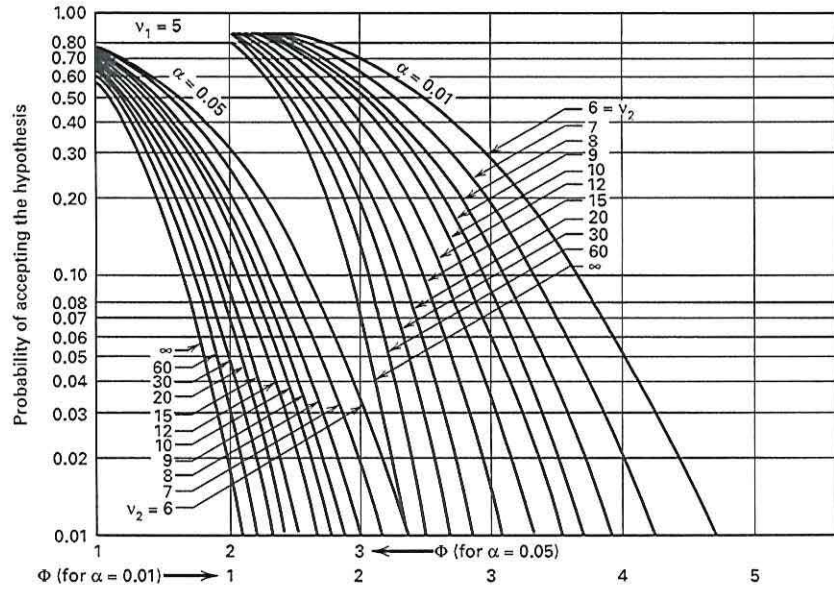


V Operating Characteristic Curves for the Fixed Effects Model Analysis of Variance (Continued)





V Operating Characteristic Curves for the Fixed Effects Model Analysis of Variance (Continued)



V Operating Characteristic Curves for the Fixed Effects Model Analysis of Variance (Continued)

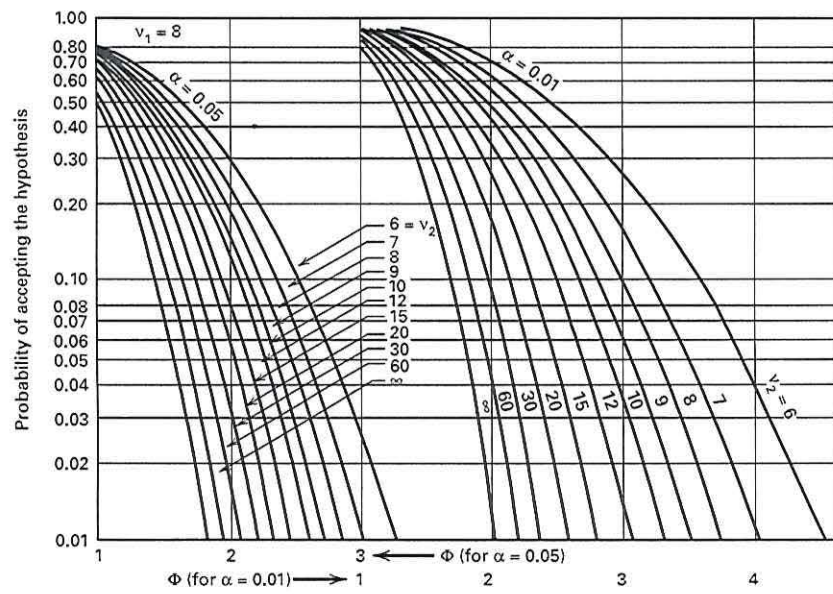
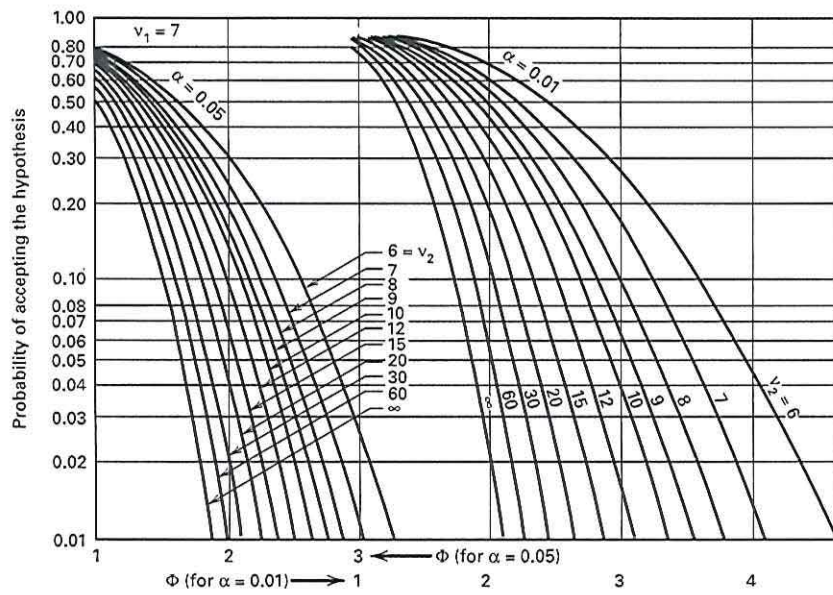
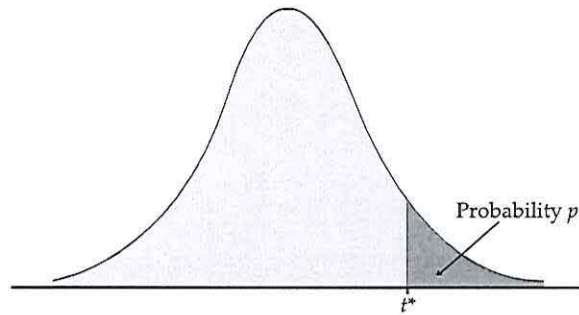


Table entry for  $p$  and  $C$  is the critical value  $t^*$  with probability  $p$  lying to its right and probability  $C$  lying between  $-t^*$  and  $t^*$ .



**TABLE D**

*t* distribution critical values

df	Upper-tail probability $p$											
	.25	.20	.15	.10	.05	.025	.02	.01	.005	.0025	.001	.0005
1	1.000	1.376	1.963	3.078	6.314	12.71	15.89	31.82	63.66	127.3	318.3	636.6
2	0.816	1.061	1.386	1.886	2.920	4.303	4.849	6.965	9.925	14.09	22.33	31.60
3	0.765	0.978	1.250	1.638	2.353	3.182	3.482	4.541	5.841	7.453	10.21	12.92
4	0.741	0.941	1.190	1.533	2.132	2.776	2.999	3.747	4.604	5.598	7.173	8.610
5	0.727	0.920	1.156	1.476	2.015	2.571	2.757	3.365	4.032	4.773	5.893	6.869
6	0.718	0.906	1.134	1.440	1.943	2.447	2.612	3.143	3.707	4.317	5.208	5.959
7	0.711	0.896	1.119	1.415	1.895	2.365	2.517	2.998	3.499	4.029	4.785	5.408
8	0.706	0.889	1.108	1.397	1.860	2.306	2.449	2.896	3.355	3.833	4.501	5.041
9	0.703	0.883	1.100	1.383	1.833	2.262	2.398	2.821	3.250	3.690	4.297	4.781
10	0.700	0.879	1.093	1.372	1.812	2.228	2.359	2.764	3.169	3.581	4.144	4.587
11	0.697	0.876	1.088	1.363	1.796	2.201	2.328	2.718	3.106	3.497	4.025	4.437
12	0.695	0.873	1.083	1.356	1.782	2.179	2.303	2.681	3.055	3.428	3.930	4.318
13	0.694	0.870	1.079	1.350	1.771	2.160	2.282	2.650	3.012	3.372	3.852	4.221
14	0.692	0.868	1.076	1.345	1.761	2.145	2.264	2.624	2.977	3.326	3.787	4.140
15	0.691	0.866	1.074	1.341	1.753	2.131	2.249	2.602	2.947	3.286	3.733	4.073
16	0.690	0.865	1.071	1.337	1.746	2.120	2.235	2.583	2.921	3.252	3.686	4.015
17	0.689	0.863	1.069	1.333	1.740	2.110	2.224	2.567	2.898	3.222	3.646	3.965
18	0.688	0.862	1.067	1.330	1.734	2.101	2.214	2.552	2.878	3.197	3.611	3.922
19	0.688	0.861	1.066	1.328	1.729	2.093	2.205	2.539	2.861	3.174	3.579	3.883
20	0.687	0.860	1.064	1.325	1.725	2.086	2.197	2.528	2.845	3.153	3.552	3.850
21	0.686	0.859	1.063	1.323	1.721	2.080	2.189	2.518	2.831	3.135	3.527	3.819
22	0.686	0.858	1.061	1.321	1.717	2.074	2.183	2.508	2.819	3.119	3.505	3.792
23	0.685	0.858	1.060	1.319	1.714	2.069	2.177	2.500	2.807	3.104	3.485	3.768
24	0.685	0.857	1.059	1.318	1.711	2.064	2.172	2.492	2.797	3.091	3.467	3.745
25	0.684	0.856	1.058	1.316	1.708	2.060	2.167	2.485	2.787	3.078	3.450	3.725
26	0.684	0.856	1.058	1.315	1.706	2.056	2.162	2.479	2.779	3.067	3.435	3.707
27	0.684	0.855	1.057	1.314	1.703	2.052	2.158	2.473	2.771	3.057	3.421	3.690
28	0.683	0.855	1.056	1.313	1.701	2.048	2.154	2.467	2.763	3.047	3.408	3.674
29	0.683	0.854	1.055	1.311	1.699	2.045	2.150	2.462	2.756	3.038	3.396	3.659
30	0.683	0.854	1.055	1.310	1.697	2.042	2.147	2.457	2.750	3.030	3.385	3.646
40	0.681	0.851	1.050	1.303	1.684	2.021	2.123	2.423	2.704	2.971	3.307	3.551
50	0.679	0.849	1.047	1.299	1.676	2.009	2.109	2.403	2.678	2.937	3.261	3.496
60	0.679	0.848	1.045	1.296	1.671	2.000	2.099	2.390	2.660	2.915	3.232	3.460
80	0.678	0.846	1.043	1.292	1.664	1.990	2.088	2.374	2.639	2.887	3.195	3.416
100	0.677	0.845	1.042	1.290	1.660	1.984	2.081	2.364	2.626	2.871	3.174	3.390
1000	0.675	0.842	1.037	1.282	1.646	1.962	2.056	2.330	2.581	2.813	3.098	3.300
$z^*$	0.674	0.841	1.036	1.282	1.645	1.960	2.054	2.326	2.576	2.807	3.091	3.291
	50%	60%	70%	80%	90%	95%	96%	98%	99%	99.5%	99.8%	99.9%
	Confidence level $C$											